

Università degli Studi di Pavia - Corso di Laurea in Ingegneria Edile e Architettura - A.A.2019/2020

Esercitazioni di
MECCANICA RAZIONALE

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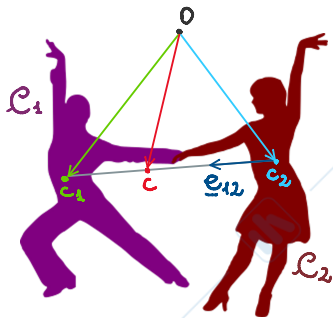
Esercitazione di Inerzia:

COMPLEMENTI DI TEORIA

1. Rappresentazione matriciale del tensore d'inerzia
2. Estensione al caso continuo
3. Riepilogo sui "trucchi di calcolo" del tensore d'inerzia
 - simmetrie materiali e basi principali
 - sistemi piani
 - Teorema di Huyg ns-Steiner
 - Teorema di Composizione (e Teorema della Lacuna)
4. Ricerca delle direzioni principali di inerzia

ESERCIZI

4) TEOREMA DI COMPOSIZIONE



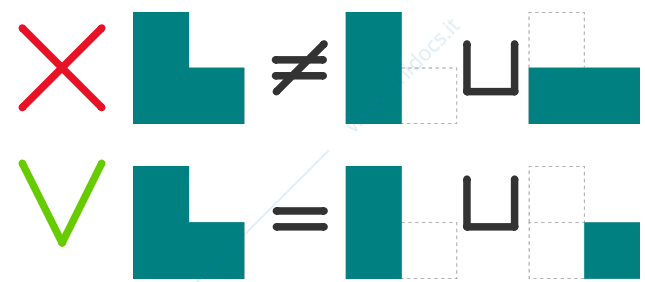
$$c - o = \frac{m_1(c_1 - o) + m_2(c_2 - o)}{m_1 + m_2}$$

$$\underline{I}_c = \underline{I}_{c_1} + \underline{I}_{c_2} + \frac{m_1 m_2}{m_1 + m_2} |c_1 - c_2|^2 (\underline{I} - e_{12} \otimes e_{12})$$

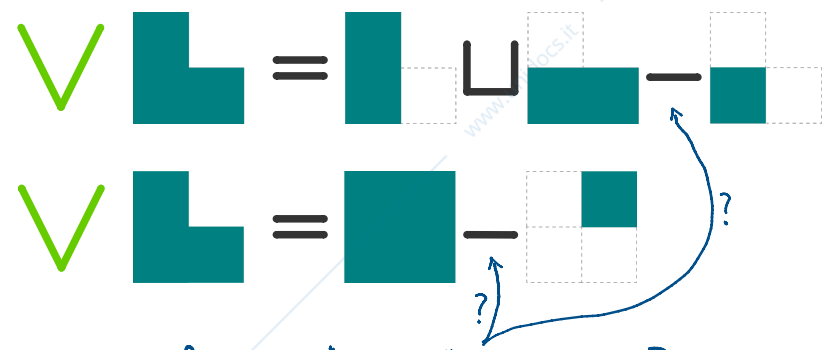
con $m(C_1 \cap C_2) = 0$ } lo indichiamo
 con
 $c = c_1 \cup c_2$ } $\underline{I} = \underline{I}_{c_1} \cup \underline{I}_{c_2}$

Nota: $m(C_1 \cap C_2) = 0 \rightarrow$ i corpi C_1 e C_2 al massimo si TOCCANO MA NON SI SOVRAPPONGONO

Esempio:



sto prendendo
2 volte
l'intersezione!



Come faccio a "sottrarre" corpi tra loro?

\rightarrow uso il Teorema di Composizione in un modo particolare:

$$\frac{(m_1 + m_2)(c - c_2)}{m} = m_1(c_1 - c_2) + m_2(c_2 - c_2) \quad e \quad \underline{I}_c = \underline{I}_{c_1} + \underline{I}_{c_2} + \frac{m_1 m_2}{m_1 + m_2} |c_1 - c_2|^2 (\underline{I} - e_{12} \otimes e_{12})$$



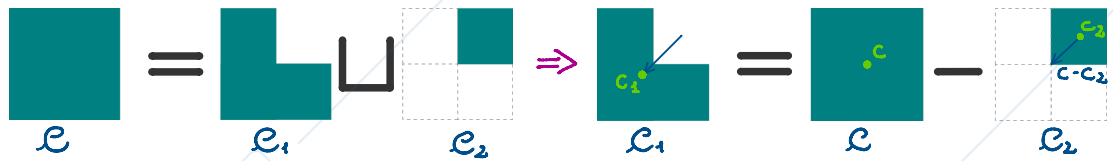
Teorema della Sottrazione:

$$c_1 - c_2 = \frac{m}{m - m_2} (c - c_2)$$

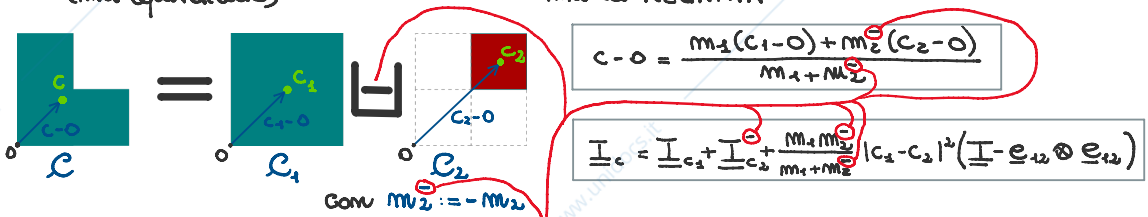
$$e \quad \underline{I}_{c_1} = \underline{I}_c - \underline{I}_{c_2} - \frac{(m - m_2)m_2}{m} |c_1 - c_2|^2 (\underline{I} - e_{12} \otimes e_{12})$$

$$= \underline{I}_c - \underline{I}_{c_2} - \frac{m - m_2}{m - m_2} |c - c_2|^2 (\underline{I} - e_{12} \otimes e_{12})$$

* Nell' Esempio:

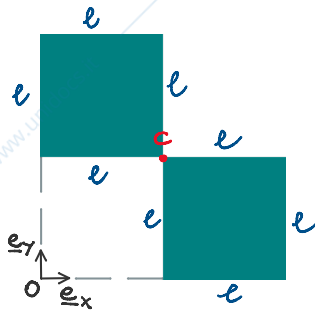


* Formulazione alternativa: "sottrarre" = "unire" corpi di massa NEGATIVA (ma equivalente)



per ricordarmi che m_2 ha segno NEGATIVO

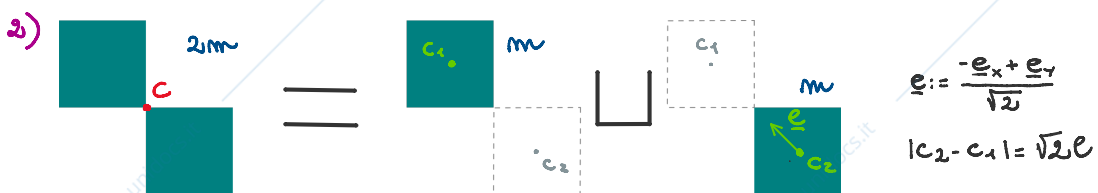
Esercizi di Inerzia: **FIGURE COMPOSTE**



massa totale: $2m$ (uniformemente distribuita)

- 1) $c-o = ?$
- 2) $I_c = ?$
- 3) $I_o = ?$

1) Per simmetria: $c-o = l e_x + l e_y$



$$\underline{I}_{c_1} = \underline{I}_{c_2} = \frac{1}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z)$$

$$\begin{aligned} \rightarrow \underline{I}_c &= \frac{1}{6} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z) + m l^2 (\underline{I} - \underline{e}_z \otimes \underline{e}_z) \\ &= \frac{7}{6} m l^2 \underline{I} - m l^2 \underline{e}_z \otimes \underline{e}_z + \frac{1}{6} m l^2 \underline{e}_z \otimes \underline{e}_z \\ &= \frac{7}{6} m l^2 \underline{I} - \frac{1}{2} m l^2 (\underline{e}_x \otimes \underline{e}_x - \underline{e}_x \otimes \underline{e}_y - \underline{e}_y \otimes \underline{e}_x + \underline{e}_y \otimes \underline{e}_y) + \frac{1}{6} m l^2 \underline{e}_z \otimes \underline{e}_z \\ &= \frac{8}{3} m l^2 \underline{e}_x \otimes \underline{e}_x + \frac{1}{2} m l^2 \underline{e}_x \otimes \underline{e}_y + \frac{1}{2} m l^2 \underline{e}_y \otimes \underline{e}_x + \frac{2}{3} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{1}{3} m l^2 \underline{e}_z \otimes \underline{e}_z \end{aligned}$$

direzione principale

* $\underline{e}_x, \underline{e}_y$ non sono direzioni principali per \underline{I}_c
* $\underline{I}_{c_{zz}} = \underline{I}_{c_{xx}} + \underline{I}_{c_{yy}}$

$$3) \underline{I}_o = \frac{7}{6} m l^2 \underline{I} - m l^2 \underline{e}_z \otimes \underline{e}_z + \frac{1}{6} m l^2 \underline{e}_z \otimes \underline{e}_z + 2 m l^2 \underline{e}_z \otimes \underline{e}_z \quad \underline{e}_1 := \frac{\underline{e}_x + \underline{e}_y}{\sqrt{2}} \perp \underline{e}_z$$

$$= \frac{35}{6} m l^2 \underline{e}_z \otimes \underline{e}_z + \frac{7}{6} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{16}{3} m l^2 \underline{e}_z \otimes \underline{e}_z \rightarrow (\underline{e}_1, \underline{e}_z) \text{ principale per } \underline{I}_o$$

$$= \frac{8}{3} m l^2 \underline{e}_x \otimes \underline{e}_x - \frac{3}{2} m l^2 \underline{e}_x \otimes \underline{e}_y - \frac{3}{2} m l^2 \underline{e}_y \otimes \underline{e}_x + \frac{8}{3} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{16}{3} m l^2 \underline{e}_z \otimes \underline{e}_z$$

TEOREMA DI COMPOSIZIONE

$$\underline{I}_c = \underline{I}_{c_1} + \underline{I}_{c_2} + \frac{m_1 m_2}{m_1 + m_2} |c_1 - c_2|^2 (\underline{I} - \underline{e}_{12} \otimes \underline{e}_{12})$$

QUADRATO

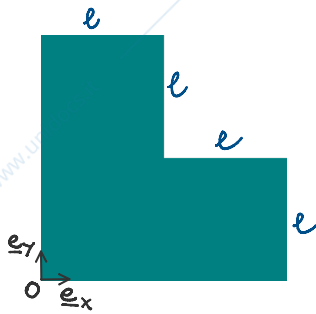
lato: l
massa: m

$$\underline{I}_c = \frac{1}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z)$$

TEOREMA DI HUYGENS-STEINER

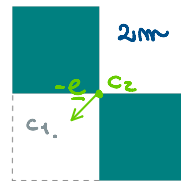
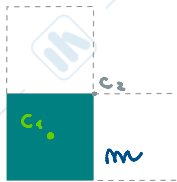
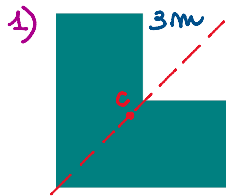
$$\underline{I}_o = \underline{I}_c + m |c - o|^2 (\underline{I} - \underline{e}_z \otimes \underline{e}_z)$$

Esercizi di Inerzia: FIGURE COMPOSTE



massa totale: $3m$ (uniformemente distribuita)

- 1) $c - o = ?$
- 2) $\underline{I}_c = ?$
- 3) $\underline{I}_o = ?$



$$\underline{e}_z = \frac{-\underline{e}_x + \underline{e}_y}{\sqrt{2}}$$

$$\underline{e}_1 := \frac{\underline{e}_x + \underline{e}_y}{\sqrt{2}} \perp \underline{e}_z$$

$$|c_2 - c_1| = \frac{\sqrt{2}}{2} l$$

$$c_1 - o = \frac{\sqrt{2}}{2} \underline{e}_1 \quad c_2 - o = \sqrt{2} \underline{e}_1$$

$$c - o = \frac{1}{3m} (m \sqrt{2} \underline{e}_1 + 2m \sqrt{2} \underline{e}_1) = \frac{5\sqrt{2}}{6} l \underline{e}_1 =$$

$$= \frac{5}{6} l \underline{e}_x + \frac{5}{6} l \underline{e}_y$$

TEOREMA DI COMPOSIZIONE

$$c - o = \frac{m_1(c_1 - o) + m_2(c_2 - o)}{m_1 + m_2}$$

$$\underline{I}_c = \underline{I}_{c_1} + \underline{I}_{c_2} + \frac{m_1 m_2}{m_1 + m_2} |c_1 - c_2|^2 (\underline{I} - \underline{e}_{12} \otimes \underline{e}_{12})$$

2) Primo modo

$$I_{c_1} = \frac{1}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z)$$

$$I_{c_2} = \frac{7}{6} m l^2 \underline{I} - m l^2 \underline{e}_x \otimes \underline{e}_x + \frac{1}{6} m l^2 \underline{e}_z \otimes \underline{e}_z$$

$$= \frac{7}{6} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{1}{6} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{1}{3} m l^2 \underline{e}_z \otimes \underline{e}_z$$

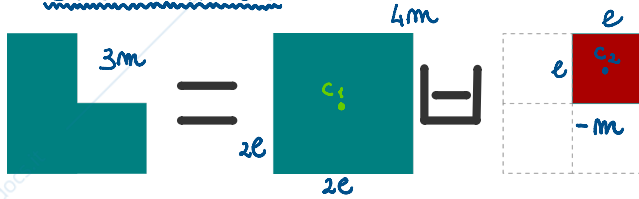
$$\rightarrow \underline{I}_c = \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{1}{4} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{3}{2} m l^2 \underline{e}_z \otimes \underline{e}_z + \frac{2}{3} m \frac{1}{2} l^2 (\underline{I} - \underline{e}_1 \otimes \underline{e}_1) =$$

$$= \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{7}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{11}{6} m l^2 \underline{e}_z \otimes \underline{e}_z$$

$$= \frac{11}{12} m l^2 \underline{e}_x \otimes \underline{e}_x + \frac{1}{3} m l^2 \underline{e}_x \otimes \underline{e}_y + \frac{1}{3} m l^2 \underline{e}_y \otimes \underline{e}_x + \frac{11}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{11}{6} m l^2 \underline{e}_z \otimes \underline{e}_z$$

Nota:  \rightarrow 3 oggetti, composti (2) alla volta

Secondo modo



$$c - o = \frac{1}{3m} (4m \sqrt{2} l \underline{e}_1 - m \frac{3}{2} \sqrt{2} l \underline{e}_y) = \frac{5}{6} \sqrt{2} l \underline{e}_1$$

$$I_{c_1} = \frac{1}{12} 4m 4l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z)$$

$$I_{c_2}^- = -\frac{1}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z)$$

$$I_c = \frac{15}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z) - \frac{4}{3} m \frac{1}{2} l^2 (\underline{I} - \underline{e}_1 \otimes \underline{e}_1)$$

$$= \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{7}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{11}{6} m l^2 \underline{e}_z \otimes \underline{e}_z$$

TEOREMA DELLA LACUNA

$$c - o = \frac{m_1(c_1 - o) + m_2(c_2 - o)}{m_1 + m_2}$$

$$I_c = I_{c_1} + I_{c_2} + \frac{m_1 m_2}{m_1 + m_2} |c_1 - c_2|^2 (\underline{I} - \underline{e}_{12} \otimes \underline{e}_{12})$$

m_2 NEGATIVA

TEOREMA DI HUYGENS-STEINER

$$I_o = I_c + m |c - o|^2 (\underline{I} - \underline{e}_z \otimes \underline{e}_z)$$

3) Primo modo

$$I_o = \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{7}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{11}{6} m l^2 \underline{e}_z \otimes \underline{e}_z + 3m \frac{25}{18} l^2 (\underline{I} - \underline{e}_1 \otimes \underline{e}_1)$$

$$= \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{57}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + 6 m l^2 \underline{e}_z \otimes \underline{e}_z$$

$$= 3 m l^2 \underline{e}_x \otimes \underline{e}_x - \frac{7}{4} m l^2 \underline{e}_x \otimes \underline{e}_y - \frac{7}{4} m l^2 \underline{e}_y \otimes \underline{e}_x + 3 m l^2 \underline{e}_y \otimes \underline{e}_y + 6 m l^2 \underline{e}_z \otimes \underline{e}_z$$

Secondo modo

$$I_o = I_o^{\square} + I_o^{\square} =$$

$$= \frac{35}{6} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{7}{6} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{16}{3} m l^2 \underline{e}_z \otimes \underline{e}_z$$

$$+ \frac{7}{12} m l^2 \underline{e}_x \otimes \underline{e}_x + \frac{1}{12} m l^2 \underline{e}_1 \otimes \underline{e}_1 + \frac{2}{3} m l^2 \underline{e}_z \otimes \underline{e}_z$$

$$= \frac{57}{12} m l^2 \underline{e}_y \otimes \underline{e}_y + \frac{5}{4} m l^2 \underline{e}_1 \otimes \underline{e}_1 + 6 m l^2 \underline{e}_z \otimes \underline{e}_z$$

Infatti: $I_o = \int (r^2 \underline{I} - \underline{r} \otimes \underline{r}) dm$
 \hookrightarrow spezzo in $\int \dots + \int \dots$

QUADRATO

$$I_o = \frac{1}{12} m l^2 (\underline{I} + \underline{e}_z \otimes \underline{e}_z) + \frac{1}{2} m l^2 (\underline{I} - \underline{e}_1 \otimes \underline{e}_1)$$

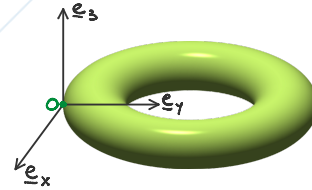
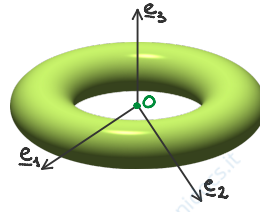
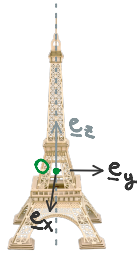
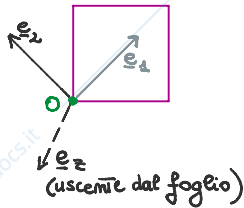
Inerzia **RICERCA DELLE DIREZIONI PRINCIPALI**

METODO (1): ricerca dei PIANI DI RIFLESSIONE → è un metodo usabile **A PRIORI** (prima di conoscere \mathbb{I}_0)

Se il PIANO $\perp e$ passante per O è di RIFLESSIONE per e ($= R_e \cdot e = e$)

⇒ e è una DIREZIONE PRINCIPALE D'INERZIA per \mathbb{I}_0

- 1) Trovo $e_1 \perp e_2$ principali usando le riflessioni ininterne
- 2) Completo la base con $e_3 := e_1 \times e_2$ (che è sicuramente principale)



METODO (2): ricerca degli AUTOVETTORI → è un metodo usabile solo **A POSTERIORI** (dopo aver calcolato \mathbb{I}_0)

Le DIREZIONI PRINCIPALI D'INERZIA sono gli AUTOVETTORI di \mathbb{I}_0 .

$$e_i \text{ principale} \Rightarrow \mathbb{I}_0 \cdot \underbrace{e_i}_{\text{autovettore}} = \underbrace{I_{0ii}}_{\text{autovalore}} e_i \quad \text{con } I_{0ii} = e_i \cdot \mathbb{I}_0 \cdot e_i$$

1) Risolvo $\mathbb{I}_0 \cdot v = \lambda v$: • $\det(\mathbb{I}_0 - \lambda \mathbb{I}) = 0 \rightarrow$ trovo gli autovalori $\lambda_1, \lambda_2, \lambda_3$

• per $i=1,2,3$ $(\mathbb{I}_0 - \lambda_i \mathbb{I}) \cdot v_i = 0 \rightarrow$ trovo gli autovettori v_1, v_2, v_3

$$v_x e_x + v_y e_y + v_z e_z$$

e trovo le relazioni che legano v_x, v_y, v_z (poi scelgo dei valori numerici che le soddisfanno)

2) Normalizzo (per ottenere dei VERSORI): $e_i := \frac{v_i}{|v_i|}$

3) Ordino (e_1, e_2, e_3) in modo che $e_3 = e_1 \times e_2$

(oppure trovo solo e_1, e_2 - controllando che $e_2 \perp e_1$ - e poi aggiungo $e_3 := e_1 \times e_2$)

METODO (3): Ricerca dei PUNTI STAZIONARI di $e \mapsto \underline{I}_0 e \mapsto$ metodo A POSTERIORI

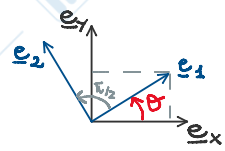
Le DIREZIONI PRINCIPALI D'INERZIA sono i PUNTI STAZIONARI della funzione

$$f(e) := \underline{I}_0 e = e \cdot \underline{I}_0 e \quad \rightarrow \text{minimi, selle, massimi}$$

Vediamo il caso 2D (C e O e piano xy)
 \rightarrow in 3D il conto e' simile, ma piu' complicato

1) Scrivo $\underline{I}_0 = I_{0xx} e_x \otimes e_x + I_{0xy} e_x \otimes e_y + I_{0xy} e_y \otimes e_x + I_{0yy} e_y \otimes e_y + I_{0zz} e_z \otimes e_z$

* e_z e' principale \rightarrow mi basta e_1 nel piano xy
 poi $e_2 := e_z \times e_1$



2) Scrivo e generico: $e := \cos\theta e_x + \sin\theta e_y$

* cerco l'angolo θ

* mi aspetto di trovare coppie di soluzioni: θ e $\theta + \frac{\pi}{2}$

3) Impongo la STAZIONARIETA':

$$\frac{\partial}{\partial \theta} (e \cdot \underline{I}_0 e) = \frac{\partial}{\partial \theta} f(e) = 0$$

$$* \underline{I}_0 e = \cos\theta (I_{0xx} e_x + I_{0xy} e_y) + \sin\theta (I_{0xy} e_x + I_{0yy} e_y)$$

$$* e \cdot \underline{I}_0 e = \cos^2\theta I_{0xx} + \underbrace{\sin\theta \cos\theta I_{0xy} + \sin\theta \cos\theta I_{0xy}}_{\sin(2\theta) I_{0xy}} + \sin^2\theta I_{0yy}$$

$$* \frac{\partial}{\partial \theta} (e \cdot \underline{I}_0 e) = 0 \Rightarrow \underbrace{-2 \sin\theta \cos\theta I_{0xx}}_{\sin(2\theta)} + 2 \cos(2\theta) I_{0xy} + \underbrace{2 \sin\theta \cos\theta I_{0yy}}_{\sin(2\theta)} = 0$$

4) Risolvo $2 \cos(2\theta) I_{0xy} = \sin(2\theta) (I_{0xx} - I_{0yy})$

CASO 1 $I_{0xx} = I_{0yy} \Rightarrow I_{0xy} \cos(2\theta) = 0$

a) $I_{0xy} = 0 \Rightarrow 0 = 0 \rightarrow$ ogni θ va bene



ogni direzione nel piano xy e' principale
 ($e \cdot \underline{I}_0 e$ era gia' in forma diagonale)

$$\underline{I}_0 = \underbrace{\frac{1}{2} I_{0zz}}_{I_{0xx} = I_{0yy}} (\underline{I} - e_z \otimes e_z) + \underbrace{I_{0zz}}_{I_{0xx} + I_{0yy}} e_z \otimes e_z \rightarrow \text{SIMMETRIA CILINDRICA}$$

b) $I_{0xy} \neq 0 \Rightarrow \cos(2\theta) = 0 \rightarrow \theta = \langle \frac{\pi}{4}, \frac{3\pi}{4} \rangle$

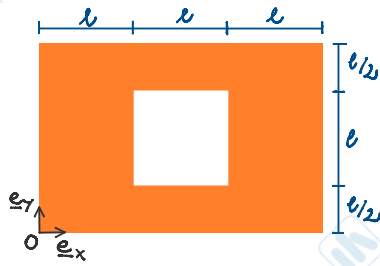


CASO 2 $I_{0xx} \neq I_{0yy} \Rightarrow \cos(2\theta) \neq 0 \rightarrow \tan(2\theta) = \frac{2 I_{0xy}}{I_{0xx} - I_{0yy}}$

$$\rightarrow \theta = \frac{1}{2} \arctan \frac{2 I_{0xy}}{I_{0xx} - I_{0yy}}$$

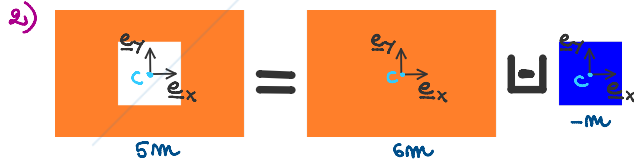
Se $I_{0xy} = 0 \Rightarrow \theta = \langle \frac{\pi}{2} \rangle \rightarrow e_x$ ed e_y erano gia' principali

Esercizi di Inerzia: FIGURE COMPOSTE E DIREZIONI PRINCIPALI



- massa totale: $5m$ (uniformemente distribuita)
 1) $c-o = ?$ 2) $I_c = ?$
 3) $I_o = ?$ 4) $I_{o, B} = ?$ con $m \parallel c-o$
 5) base principale di $I_o = ?$

1) Per simmetria $c-o = \frac{3}{2}l e_x + l e_y$ e (e_x, e_y, e_z) principale per I_c



$c_1 \equiv c_2 \equiv c \Rightarrow c_1 - c_2 = 0$
 $I_{c_1} = \frac{1}{12} 6m 4l^2 e_x \otimes e_x + \frac{1}{12} 6m 9l^2 e_y \otimes e_y + \frac{1}{12} 6m 13l^2 e_z \otimes e_z$
 $I_{c_2} = -\frac{1}{12} m l^2 e_x \otimes e_x - \frac{1}{12} m l^2 e_y \otimes e_y - \frac{1}{6} m l^2 e_z \otimes e_z$

$I_c = \frac{23}{12} m l^2 e_x \otimes e_x + \frac{53}{12} m l^2 e_y \otimes e_y + \frac{19}{3} m l^2 e_z \otimes e_z$

TEOREMA DELLA LACUNA
 $c-o = \frac{m_1(c_1-o) + m_2(c_2-o)}{m_1+m_2}$
 $I_c = I_{c_1} + I_{c_2} + \frac{m_1 m_2}{m_1+m_2} |c_1-c_2|^2 (I - e_{12} \otimes e_{12})$
 m_2 NEGATIVA

RETTANGOLO

 massa: m
 $I_c = \frac{1}{12} m b^2 e_x \otimes e_x + \frac{1}{12} m a^2 e_y \otimes e_y + \frac{1}{12} m (a^2 + b^2) e_z \otimes e_z$

3) $m = \frac{c-o}{|c-o|} = \frac{\frac{3}{2}e_x + e_y}{\sqrt{13/4} l} = \frac{3}{\sqrt{13}} e_x + \frac{2}{\sqrt{13}} e_y$
 $|c-o|^2 = \frac{13}{4} l^2 = \frac{1}{\sqrt{13}} (3e_x + 2e_y)$

TEOREMA DI HUYGENS-STEINER
 $I_o = I_c + m |c-o|^2 (I - e \otimes e)$

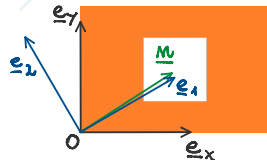
$I_o = \frac{23}{12} m l^2 e_x \otimes e_x + \frac{53}{12} m l^2 e_y \otimes e_y + \frac{19}{3} m l^2 e_z \otimes e_z + 5m \frac{13}{4} l^2 [I - \frac{1}{13} (3e_x + 2e_y) \otimes (3e_x + 2e_y)]$
 $= (\frac{23}{12} + 5) m l^2 e_x \otimes e_x - 5 \frac{3}{2} m l^2 e_x \otimes e_y - 5 \frac{3}{2} m l^2 e_y \otimes e_x + (\frac{53}{12} + 5 \frac{9}{4}) m l^2 e_y \otimes e_y + (\frac{19}{3} + 5 \frac{13}{4}) m l^2 e_z \otimes e_z$
 $= \frac{83}{12} m l^2 e_x \otimes e_x - \frac{15}{2} m l^2 e_x \otimes e_y - \frac{15}{2} m l^2 e_y \otimes e_x + \frac{188}{12} m l^2 e_y \otimes e_y + \frac{871}{12} m l^2 e_z \otimes e_z$

4) $I_{o, B} = m \cdot I_o \cdot m = \frac{1}{13} (3e_x + 2e_y) \cdot [(\frac{83}{4} - 15) e_x + (\frac{94}{3} - \frac{45}{2}) e_y] m l^2$
 $= \frac{1}{13} (\frac{69}{4} + \frac{53}{3}) = \frac{1}{13} \cdot \frac{419}{12} = \frac{419}{166}$

definizione
MOMENTO ASSIALE:
 $I_{o, u} = u \cdot I_o \cdot u$

5) $B = (e_1, e_2, e_3)$ con $e_1 = \cos \theta e_x + \sin \theta e_y$, $e_2 = -\sin \theta e_x + \cos \theta e_y$

dove $\theta = \frac{1}{2} \arctan \frac{2I_{oxy}}{I_{oxx} - I_{oyy}}$
 $= \frac{1}{2} \arctan \frac{12}{7}$



DIREZIONI PRINCIPALI in 2D
 $B = (e_1, e_2, e_3)$
 $e_1 = \cos \theta e_x + \sin \theta e_y$, $e_2 = e_3 \times e_1$
 $I_{oxx} = I_{oyy}$ e $I_{oxy} = 0 \rightarrow \forall \theta$
 $I_{oxx} \neq I_{oyy}$ e $I_{oxy} \neq 0 \rightarrow \theta = \pi/4$ e $\theta = 3\pi/4$
 $I_{oxx} + I_{oyy} \rightarrow \theta = \frac{1}{2} \arctan \frac{2I_{oxy}}{I_{oxx} - I_{oyy}}$